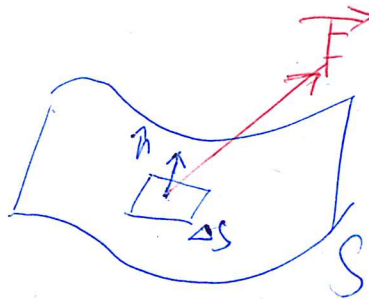


Surface Integrals

$$\iint_S f dS \quad \text{or} \quad \iint_S \vec{F} \cdot \hat{n} dS$$



Computation:

Find dS and $d\vec{S} = \hat{n} \cdot dS$

(1) When S is parametrized: $\vec{r}(u,v) = \langle x(u,v), y(u,v), z(u,v) \rangle$

$\hat{n} dS = \pm (\vec{r}_u \times \vec{r}_v) du dv$
$dS = \ \vec{r}_u \times \vec{r}_v\ du dv$

Example: graph: $\vec{r}(x,y) = \langle x, y, f(x,y) \rangle$
 $r_x = \langle 1, 0, f_x \rangle$, $r_y = \langle 0, 1, f_y \rangle$

$$\Rightarrow \hat{n} dS = \pm \langle -f_x, -f_y, 1 \rangle dx dy$$

(2) When S is given by an equation $g(x,y,z) = 0$

$$\vec{N} = \nabla g, \quad \text{and} \quad \hat{n} = \pm \frac{\vec{N}}{|\vec{N}|}$$

$dS = \frac{ \vec{N} }{\vec{N} \cdot \hat{k}} dx dy$
$\hat{n} \cdot dS = \pm \frac{\vec{N}}{ \vec{N} } dx dy$

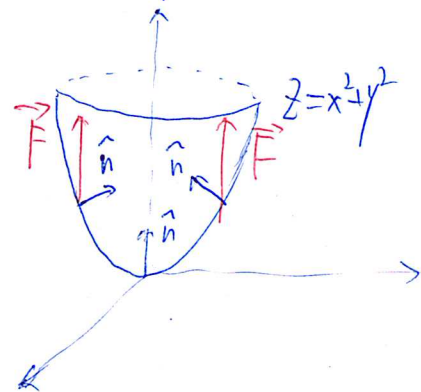
Example: graph: $g(x,y,z) = z - f(x,y) = 0$

$$\vec{N} = \nabla g = \langle -f_x, -f_y, 1 \rangle$$

$$\Rightarrow \hat{n} dS = \pm \langle -f_x, -f_y, 1 \rangle dx dy$$

Example: $\vec{F} = z\hat{k}$ $S =$ portion of paraboloid $z = x^2 + y^2$ above unit disk, \hat{n} upwards

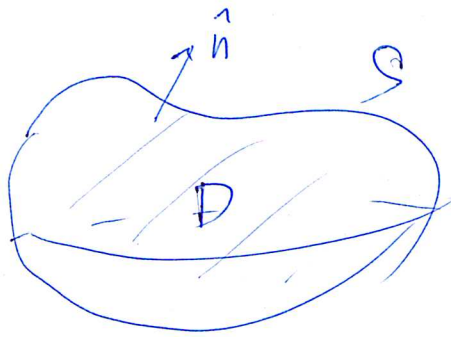
$$\begin{aligned} \iint_S \vec{F} \cdot \hat{n} dS &= \iint_S \langle 0, 0, z \rangle \cdot \langle -2x, -2y, 1 \rangle dx dy \\ &= \iint_S z dx dy \\ &= \iint (x^2 + y^2) dx dy \\ &= \int_0^{2\pi} \int_0^1 r^2 \cdot r dr d\theta = \frac{\pi}{2} \end{aligned}$$



$$\begin{aligned} \text{Area}(S) &= \iint_S dS = \iint \sqrt{1 + 4x^2 + 4y^2} dx dy = \int_0^{2\pi} \int_0^1 \sqrt{1 + 4r^2} r dr d\theta \\ &= \frac{\pi}{6} (5\sqrt{5} - 1) \end{aligned}$$

Divergence Theorem

S closed surface enclosing D
oriented with \hat{n} outwards



\vec{F} defined everywhere in D .

Then,
$$\oiint_S \vec{F} \cdot \hat{n} dS = \iiint_D \text{div} \vec{F} dV$$

Physical intuition:
the amount of fluid generated by sources in D
= the amount of fluid flows out of S .

where

$$\text{div} \langle P, Q, R \rangle = P_x + Q_y + R_z$$

Proof: (1) Simplify integrand: only need to prove $\oiint_S \langle 0, 0, R \rangle \cdot \hat{n} dS = \iiint_D R_z dV$
(then get the general case by summing three such identities, one for each component)

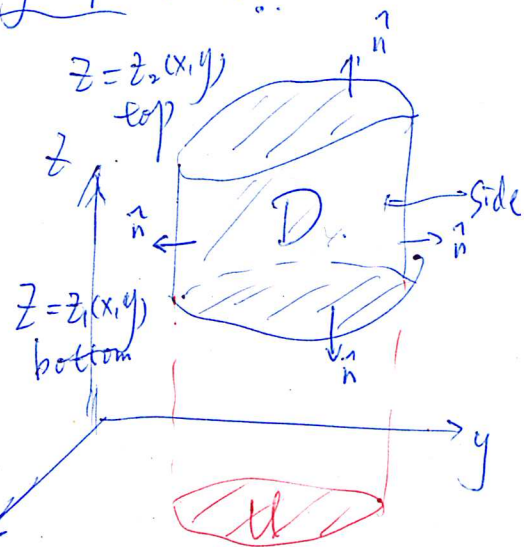
(2) Simplify domain: decompose D into vertically simple domains.

Prove the identity for each small piece,
and sum together to get the general case.

(3) Main part: $\vec{F} = \langle 0, 0, R \rangle$ on vertically simple D

$$- \iiint_D R_z dV = \iint_U \left(\int_{z_1(x,y)}^{z_2(x,y)} R_z dz \right) dx dy$$

$$= \iint_U (R(x,y, z_2(x,y)) - R(x,y, z_1(x,y))) dx dy$$



$$- \oiint_S = \iint_{\text{top}} + \iint_{\text{bottom}} + \iint_{\text{sides}} = \iint_U R(x,y, z_2(x,y)) dx dy - \iint_U R(x,y, z_1(x,y)) dx dy$$

$$\iint_{\text{top}} = \iint_{\text{top}} \langle 0, 0, R \rangle \cdot \left\langle -\frac{\partial z_2}{\partial x}, -\frac{\partial z_2}{\partial y}, 1 \right\rangle dx dy = \iint_U R(x,y, z_2(x,y)) dx dy$$

$$\iint_{\text{bottom}} = \iint_{\text{bottom}} \langle 0, 0, R \rangle \cdot \left\langle +\frac{\partial z_1}{\partial x}, +\frac{\partial z_1}{\partial y}, -1 \right\rangle dx dy = -\iint_U R(x,y, z_1(x,y)) dx dy$$

$$\iint_{\text{sides}} = 0 \quad \text{since } \langle 0, 0, R \rangle \text{ is tangent to sides.} \quad \square$$

∇ notation: ∇ "del" = $\langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \rangle$.

• $\nabla f = \langle \frac{\partial f}{\partial x}, \frac{\partial f}{\partial y}, \frac{\partial f}{\partial z} \rangle$ gradient

• $\nabla \cdot \vec{F} = \langle \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \rangle \cdot \langle P, Q, R \rangle = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y} + \frac{\partial R}{\partial z}$ divergence.

• $\nabla^2 f = \nabla \cdot (\nabla f) = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2}$ Laplacian.

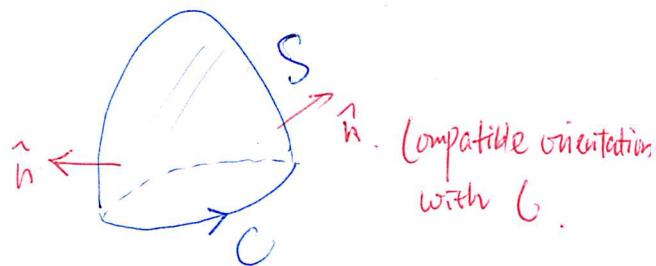
• $\nabla \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ P & Q & R \end{vmatrix} = \langle \frac{\partial R}{\partial y} - \frac{\partial Q}{\partial z}, \frac{\partial P}{\partial z} - \frac{\partial R}{\partial x}, \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \rangle$ curl

Stokes' theorem

C closed curve

S any surface bounded by C .

\vec{F} defined everywhere on S .

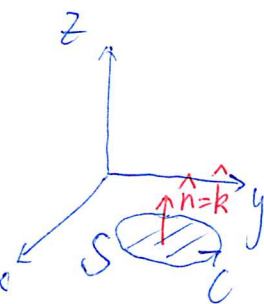


Then $\oint_C \vec{F} \cdot d\vec{r} = \iint_S \text{curl } \vec{F} \cdot \hat{n} \, dS$

Idea of proof: - True for C, S in xy -plane

$$\oint_C \vec{F} \cdot d\vec{r} = \oint_C P dx + Q dy = \iint_S (Q_x - P_y) dx dy = \iint_S (\nabla \times \vec{F}) \cdot \hat{n} \, dS$$

(Green's thm) $\hat{n} = \hat{k}$



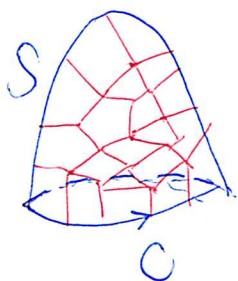
- True for C, S in any plane,

because work, flux, curl make sense indep. of coordinate system.

- Given any S , decompose it into tiny, almost flat pieces.

Sum of flux through each piece = total flux through S

Sum of work around each piece = total work along C .



Physical Applications

1. Maxwell's equation

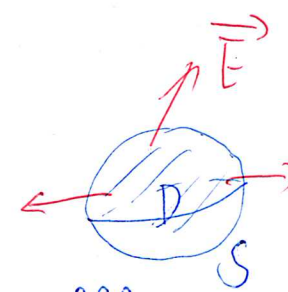
- Gauss-Columb law: $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$ (const)

electric charge density

divergence thm


flux of E out of S .

$\oint_S \vec{E} \cdot \vec{n} dS = \iiint_D \nabla \cdot \vec{E} dV = \frac{1}{\epsilon_0} \iiint_D \rho dV = \frac{Q}{\epsilon_0}$ ← electric charge in D .


- Faraday's law: $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$ (Stokes thm)

electric charge in D .

$\oint_C \vec{E} \cdot d\vec{r} = \iint_S (\nabla \times \vec{E}) \cdot d\vec{S} = \iint_S -\frac{\partial \vec{B}}{\partial t} \cdot d\vec{S} = -\frac{d}{dt} \iint_S \vec{B} \cdot d\vec{S}$ ← flux of magnetic field.


- Gauss law: $\nabla \cdot \vec{B} = 0$
- Ampère's law: $\nabla \times \vec{B} = \mu_0 \vec{J} + \epsilon_0 \mu_0 \frac{\partial \vec{E}}{\partial t}$ (const)

vector current density

"Voltage"

2. Diffusion/Heat equation

u = concentration/temperature at a given pt at a given moment
 $= u(x, y, z, t)$

Satisfies: $\frac{\partial u}{\partial t} = k \nabla^2 u = k \nabla \cdot \nabla u = k \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$ (const)

Why this equation? Let Flow of smoke = \vec{F} .

- Smoke flow from high concentration to low concentration.

\vec{F} direct along $-\nabla u$

In fact, reasonable to assume $\vec{F} = -k \nabla u$ for some const k .

- Relate \vec{F} and $\frac{\partial u}{\partial t}$ using divergence thm.

Flow out of D through S is



$$\begin{aligned} \iiint_D \operatorname{div} \vec{F} dV &\stackrel{\substack{\text{divergence} \\ \text{thm}}}{=} \oint_S \vec{F} \cdot \hat{n} dS = \text{Amount of smoke through } S \text{ per unit time} \\ &= -\frac{d}{dt} \left(\iiint_D u dV \right) \\ &= -\iiint_D \frac{\partial u}{\partial t} dV \end{aligned}$$

↑ Amount of smoke contained in D

Hence, for any D , $\iiint_D \operatorname{div} \vec{F} dV = -\iiint_D \frac{\partial u}{\partial t} dV$.

$$\Rightarrow \boxed{\operatorname{div} \vec{F} = -\frac{\partial u}{\partial t}}$$

Therefore, $\frac{\partial u}{\partial t} = -\operatorname{div} \vec{F} = -\operatorname{div}(-k \nabla u) = k \nabla^2 u$ □

3. Archimede's principle

Suppose a body is fully or partially submerged in a fluid, there is a buoyant force \vec{F} acts on the body.

Then, \vec{F} is upwards; $|\vec{F}| = \text{weight of the fluid displaced by the body}$.